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TECHNICAL REPORT

THEODOLITE SURVEY FOR POSITIONING THE ANTENNA FEEDS AND RESULTING POINTING ERRORS OF THE GMRT ANTENNAS IN ELEVATION.

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24/11/98

Keywords: GMRT Antennas; Pointing in elevation of GMRT antennas; Feed positioning; FPS; Theodolite Survey - antenna Feeds; Antennas - elevation pointing.

SUMMARY

This report describes results of a theodolite survey carried out during November-December 1997 for determining the angular positions of the 327 MHz feeds in the CALIBRATION POSITION of the feed Cage, i.e. when the feed cage stops as the micro-switch near 275° is hit. The procedures followed for the survey and for calculating the required COUNTS of the incremental encoder of the Feed Position System (FPS) for accurate pointing of the 237, 610/235, 150 and 1420 MHz feeds is also described. It is shown that the above procedure correctly positions the antenna feeds near the focus of the dish and also results in correct pointing of the antennas in elevation. It is estimated that this theodolite survey should result in pointing errors of the antennas in elevation of less than about \pm 3 arcmin. But this will be a fixed offset error for each frequency and can be reduced by repeated astronomical calibrations on strong sources away from galactic place.

The validity of the above procedure verified by comparing the values of the astronomical pointing errors of the antennas determined in May 1998 for 7 antennas by Observers with the offset values of the elevation encoder equal to the stowlock position minus $90^{\circ}.00$. It may be noted that each of the GMRT antennas is expected to be at $90^{\circ}.00$ in elevation in the stowlock position, within about ± 1.5 arcmin, because of the procedure that was followed for adjusting the wire-mesh surface of the antennas during their erection.

Recommendations are also made for future work.

1. INTRODUCTION

The primary antenna feeds of the 45-m parabolic dishes of GMRT are located on a square turret box, called the Feed Cage which is located just above the focus of each parabolic dish. The Feed Cage can be rotated from about 285° to -15° using a 0.5 HP DC motor controlled by a Feed Position System (FPS) which is installed at the base of each antenna (M.R. Sankararaman et.al., 1999). Fig. 1 gives the relative location of the 1420, 150, 610/233, 327 MHz feeds for the cage when the 327 MHz feed is placed at the focus of the dish. The feed at 50 MHz is still under development and will be fixed in position to the quadripods legs.

For the sake of economy, it was decided in 1992 to use an incremental encoder for determining the angular positions of the Feed Cage. The electronics of the incremental encoder is still not backed up by a non-volatile memory chip connected to a Lithium battery. Hence it becomes necessary to reset and calibrate the incremental encoder to a given CALIBRATION (CAL) value. This CAL value is taken as 17,000 counts, for the position of the Feed Cage when it hits the micro-switch located at an angle of about 275° with respect to the centre of the Feed Cage.

Unfortunately, the 275° microswitches are not located for all antennas at the same angle. Their positions vary from about 270° to 280°. The Feed Cages can be rotated from control room using FPS from N-5° to N275° within about one minute of time (N means near about). Micro-Switches are located near about 285°, 275°, -5° and -15°. Rotation can take place beyond N275° or below N-5° only if the concerned microswitches are bad. The switches at N285° and N-15° are end limit switches beyond which the cage must not get rotated for avoiding twisting and breakage of the 230 V AC power line and the receiver coaxial cables.

When the square turret of the Feed Cage is rotated to 270°.00 after CAL, the phase center of the 327 MHz feed are required to coincide with the prime focus of the 45-m dish, within an error of about cm with a jutter of only about 3 or 4 mm. Similarly,

phase-centres of the 610/235, 150 and 1420 MHz feeds would be at prime focus, when the Feed Cage is rotated to $180^{\circ}.00$, $90^{\circ}.00$ and $0^{\circ}.00$ respectively. There would arise additional error if the stools supporting the feeds are not perpendicular to the mounting plates of the Feed Cage Turret Box. The overall errors are likely to be within about ± 3 arcmin but it should be stressed that this would be a fixed error for each antenna and hence of not much consequence.

In Section 2 we discuss briefly the procedure for determining the position of the 327 MHz feed in the CAL position.

In Section 3 we describe the measurements and results of the theodolite survey which was carried out during November-December 1997 for determining the positions of 327 MHz feeds for 8 of the 30 GMRT antennas.

In Section 4 is presented a comparison of the pointing errors ("astronomical offset") of 7 out of the 8 antennas measured in May 1998 by Observers (and astronomers) with the theodolite offset values of the elevation encoders in the stowlock position which are given by the actual encoder readings in the stowlock position minus 90°.00.

Conclusions and recommendations are given in Section 5.

2. THEODOLITE MEASUREMENTS AND RELATIONS FOR CALCULATING ENCODER COUNTS

Firstly, the 45-m dish is put on the stowlock position and the Feed Cage is rotated to hit the CAL micro-switch at N-275°. We then measure the elevation and azimuth angles of the centre of the cross dipoles of the 327 MHz feed within about 10 or 20 arcsec using a theodolite placed at the apex of the dish. (Enclosure-1 for recommended procedure). Using this angle called $\theta_{\rm m}$, we then calculate the required value of the COUNT of the encoders so that the 327 MHz feed can be placed at 270°.00 within about \pm 2 arcmin. (Enclosure-2) Since all the other three feeds are located on a square turret,

phase-centres of the 610/235, 150 and 1420 MHz feeds would be at prime focus, when the Feed Cage is rotated to $180^{\circ}.00$, $90^{\circ}.00$ and $0^{\circ}.00$ respectively. There would arise additional error if the stools supporting the feeds are not perpendicular to the mounting plates of the Feed Cage Turret Box. The overall errors are likely to be within about ± 3 arcmin but it should be stressed that this would be a fixed error for each antenna and hence of not much consequence.

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they would automatically get positioned at $180^{\circ}.00$, $90^{\circ}.00$ and $0^{\circ}.00$ in the 610/235, 150 and 1420 MHz respectively (See Figs. 1 & 2). The equations used for calculating the required counts of the encoder, using values of θ_m for point positioning the feeds at prime focus are described in Enclosure-2.

3. THEODOLITE SURVEY CARRIED OUT BY SHRI WAMAN IN NOVEMBER-DECEMBER 1997 FOR 8 ANTENNAS

Theodolite survey was carried out by Shri Waman under guidance by myself and Shri Rajamohan for determining positions of 327 MHz feeds for 8 of the 30 GMRT antennas. I climbed upto the Apex for one antenna and verified the procedure when myself, S/Shri Waman, Rajamohan and Kailash Gaikwad took independent readings. These were all within 30 arcsec. The results of the measurements are given in Enclosure-3. A summary is given on Page 1 of the enclosure. The procedure followed is nearly the same as given in Enclosure-1. I have suggested taking elevation angles of Node No.12 for 8 PRF numbers rather that 4 PRF numbers. It may be noted that Shri Waman had found an error in the Face Left and Face Right of the Theodolite for elevation axis so that the readings differed by 3 arcmin, as may be seen from page 2 of Enclosure-3

4. COMPARISON OF ELEVATION OFFSET FROM ASTRONOMICAL CALIBRATIONS V/S THEODOLITE SURVEY OF THE FEED CAGE.

In Column (2) of Table 1 we have listed OFFSET values determined by observers as of 13th May 1998 for 7 out of 8 antennas surveyed by Shri Waman. For CO1, astronomical offset were not available.

In Column (3) are given Elevation Encoder values in the stowlock position as determined by observers using a programme written by Prof. V.K. Kulkarni to determine the mean value, minimising the effect of backlash due to gaps between the stowlock box

and stowlock pin (the antennas are rotated slowly from about 89° to 91° and back several times and a mean value is taken).

In Column (4) are given "Theodolite Survey OFFSET" equal to (90° - E1. encoder reading in the stowlock position).

In Column (6) are given the difference of (Theodolite - OFFSET) - (Astronomical OFFSET) for elevation axis. The differences are less than $1/10^{th}$ of antenna beamwidth at 327 MHz. Improved Astronomical Calibration for CO9, C10, C11 may give smaller differences. It is important to make astronomical calibrations for 1420 MHz as the antenna beamwidth is only about 20 arcmin and then taking average of several readings. Since stowlock position can be readily determined, it is advisable to use the value of OFFSET = (Elev. encoder reading in Stow position) - 90° for frequencies upto 600 MHz, and use astronomical calibration values only for fine tuning for the 21 cm feed, if required.

5. CONCLUSIONS AND RECOMMENDATIONS

As can be seen from Table-I that the difference between the Offset values calculated from astronomical calibration and from theodolite surveys at 327 MHz feeds (column 2 & 4 respectively) differ by about only \pm 3 arcmin. for 4 antennas but by 6 to 8 arcmin for the other 3 out of 7 antennas measured by Shri Waman during November-December 1997. The larger errors of 6 to 8 arcmin are only $1/10^{th}$ of the beamwidth of the 45-m dish at 327 MHz and could have arisen due to errors in astronomical calibrations. However, this aspect needs to be verified.

My recommendations are as follows:

a) To carryout the theodolite survey expeditiously over the next 4 to 5 weeks for 13 antennas where FPS has been installed but the theodolite survey was not done by Shri Waman. Table-2 gives summary of Shri Waman's measurements for 8 antennas.

Since the recommended procedure for the theodolite survey (Encl. 1) does not require any servo engineers or FPS engineers or technicians, it should be possible to survey at least one antenna if not two antennas during one day because the main jobs are to put the antenna in stowlock position from the control room or from the shell, climb the antenna, mount the theodolite, adjust it and take readings in azimuth and elevation of 8 parabolic frames and finally readings of the 327 MHz cross dipoles, both in Face Left and Face Right 3 or 4 times. In fact, it is only a two or three hours job!

- b) It is very important to record in a register or a special "pointing measurement file" any changes made to the N275 Microswitch used for calibration. The workers and engineers should give in writing that that the microswitch has been replaced exactly in the same position within 1/2 mm or better by putting a scratch line on either side of the microswitch before it is removed and refitting it accordingly. This report must be submitted to the Control room to Professor-in-Charge very promptly.
- c) It is extremely important that readings are recorded systematically in a tabular form and consistency checked before one climbs down from the antenna. The analysis can be done at Khodad or Pune at a later date but within a week.
- d) It is also very important that prompt notification is recorded in a file in the control room in case if any elevation encoder or its black box is removed from the antenna. It is highly desirable to take readings of the elevation encoders prior to removing the encoders or soon after on the same day or within the next day. Copies of the works carried on the encoders may be sent to the control room, Prof. A.P. Rao and Prof. V.K. Kulkarni. I would appreciate getting a copy of the same over the next 3 months. I would also appreciate if xerox copy of the past history of replacement of encoders is sent to me because I want to study the changes in the stowlock position for the last two years. While there are step changes in many cases, possibly because of replacement of encoders, there also seems to be some ups and downs in the stowlock position encoder readings for a few antennas, possibly due to loose couplings

(Enclosure-3). It is not possible to do astronomical calibrations frequently and hence stability of encoders is extremely important.

- e) It is also desirable to take elevation encoder readings for the stowlock positions of all the antennas using programme by Prof. V.K. Kulkarni every fortnight so that we can study the stability of the elevation encoders in the stowlock positions.
- f) We may also decide whether we should use counts or degrees (two decimals) for Feed positions. I prefer the latter so that it is immediately obvious as to which Feed is pointed to the dish. The Offset of Feed encoders for 327 MHz can be made hidden to astronomers. However, a programme is being written for both counts and degrees as per relations given in Enclosure-2.

6. ACKNOWLEDGMENTS:

I acknowledge thanks to Shri S. Rajamohan, who got the survey done by Shri Waman and other staff and Observers for various aspects of this report.

Sankeraman et al (1999): Feed Position System.

J GMAS : Technical Report, under preparation.

1999.

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Table 1: Comparison of Astronomical Calibration of Elevation Encoder with the values of Elevation Encoder in the Stowlock Position for Seven antennas Surveyed by Waman during November-December 1997

Sr. No.	Ant	OFFSET * Astronomical (13 th May 97)+	Stowlock Position Elev.Encod Reading	dolite	of sto Meas	w +	Error or Difference ((6)-90° = (4)-(2)
	1	2	3	4	5	6	7
1.	C04	-5'	89° 58'	-2'	19.4.98	90° 03'	+03'
2.	C05	-11'	89° 49'	-11'	19.4.98	90° 00'	.00'
3.	C06	0°	89° 57'	-3'	15.9.97	89° 57'	-03'
4.	C08	10'	90° 08'	8'	19.4.98	89° 58'	-02'
5.	C09	-37'	89° 17'	-43'	19.4.98	89° 54'	-06'
6.	C10	28'	90° 20'	20	19.4.98	89° 52'	-08
7.	C11	18'	90° 12'	12'	19.4.98	89° 54'	-06'

^{*} OFFSET = True-(Stowlock position elevation encoder reading)
(as per Prof. V.K. Kulkarni)

Therefore, True = (Stowlock position E1. Encoder Reading - Offset)

Since the Feed Cages have been surveyed by Shri Waman for these 7 antennas and 327 MHz feed for each has been accordingly placed at the Focus using FPS, true Reading should be $90^{\circ} \pm 3$ arcmin.

- + Offset values taken from the printout by observers dt. 13.5.1997 enclosed (Table-3)
- ** The difference = error, is relatively large for some antennas. It could be due to errors in astronomical calibration since the beamwidth of GMRT antennas is about 83 arcmin and hence errors of 1/10th to 1/20th of the beamwidth could arise depending on the source flux density etc. In future we should take average of several astronomical calibrations, particularly at 21 cm.

TABLE 2 Table 2 - REPORT OF FEED POSITION CHECKING-- SURVEY WORK-- DATE -NOV. 1997 - TO -DEC: 1997 REQD. FEED POSITION 1867% CAGE CENTER D FEED CAGE CENTER _1876mid FOCAL BOINT LIMIT SW (CAZIBRATE POSITION) (FOCUS) 327 MHZ FEED CROSS DIPOLE 909 12 FOCAL POINT see Fig. 1 = 18128·6mm · 18540mm (THEODOUTE) THEODOPITE (AS PER PRW.) Notehur d2 = 181286 1867 = 9.71 00 21 00 EODOLITE THEODOLITE HERE 411.4mm APEX POINT ABLE 2 APEX POINT FEED. POSITION REQD. OFFSET (ACTUAL OFFSET OFFSET ANGLE TOWER PROBLEM SWITCH LIMIT 00° 15' 16" C-O 00° 31' 00" 00° 46' 16" C-1 SYSTEM -ROATATION - PROBLEM OF C-2 X SHSTEM ~ ROATATION - PROBLEM OF 00° 22' 00" X_{ϵ} C-3 00° 31° 00" 00° 53' 00' 00° 07' 25" C-4 ML 00" 31' 00" 00° 38' 25" 00° 30' 16" C-6 NL 00" 31' 00" 01° 16" 01 C-8 00° 29' 03" ŊĹ 00° 51'00" 01° 00' 03" C-9 <u>00° 01′ 05″</u> πΩL 31,00, 32' 05" 00, 00° 11/1 C-10 00° 04' 58" 00, 31, 00, 00° 35′ 58″ M C-11 PROBLEM -WITCH - LIMIT C-13 te lhebe - HONY BEEHAVE 00° 22' 45" C-14 00° 31' 00" 53'45" C-5 ೲ

SURFACE MEASURMENT WORK

C-13

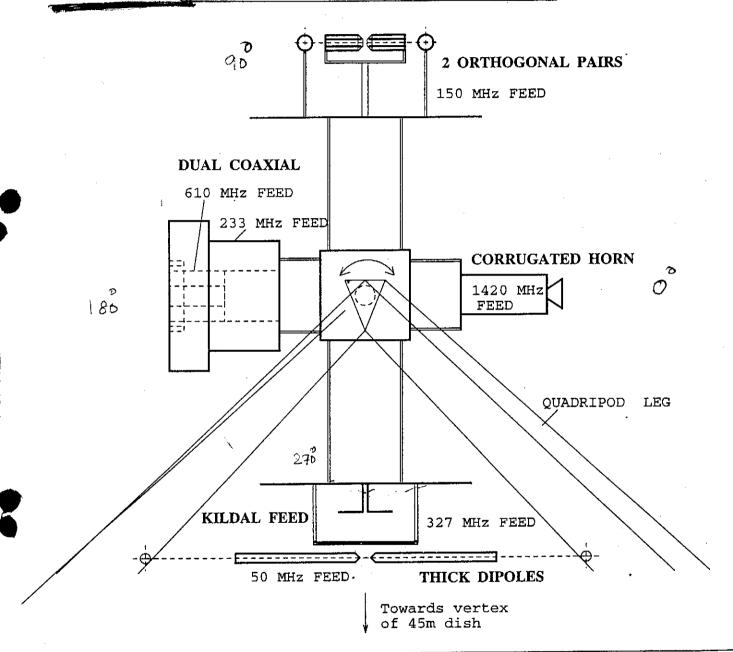
REPORT BHALCHAND

OVER

Table 3 OFFSET (as per Observers (13 Hay 98).

```
DATE 13may98
     Current antenna offset f
     subar 0
      *C04
      cp 0; ante 1 3; defs 0;
      1dantof(3', -5')
      C09
      cp 0;ante 1 4; defs 0;
      1dantof(5', -37')
      *C02
      cp 0;ante 1 5; defs 0;
      ldantof(3d24',18')
0
      *C00
      cp 0;ante 1 7; defs 0;
      1dantof(30',-27')
      *C11
      cp 0; ante 1 9; defs 0;
      ldantof(-30', 18')
      *C14
      cp 0; ante 1 10; defs 0;
      ldantof(30', 21')
      *CI3
      cp 0;ante 1 11; defs 0;
      ldantof(28', 35')
       *C10
      cp 0; ante 1 12; defs 0
      ldantof(2d12', 28')
      cp 0;ante 1 19; defs 0;
      ldantof(8d20', -11')
      *C06
      cp 0; ante 1 20; defs 0;
      ldantof(0d,0d)
       *C08
       cp 0; ante 1 24; defs 0;
       ldantof(42',10')
       *S03
      ante 1 27; defs 0
       ldantof(7',-20')
```

FIG. | GMRT PRIME FOCUS FEEDS



Parameters	50 MHz	150 MHz	233 MHz	327 MHz	610 MHz	1420 MHz
Taper w/o space loss	-8.6 ± 1 dB	-9 + 1 dB	-9 + 0.5 dB	-12.2 + 1 dB	-9.8 ± 1 dB	-19 dB
Cross-polar peak		-17.4 dB	4 4 8	-27.5 dB	-22.8 dB	-24 dB
Side lobe level	-9 ± 1 dB	-22 + 4 dB	-15 ± 1 dB	-22 + 4 dB	-17 + 3 dB	
Aperture efficiency	0.515	0.718	0.693	0.742	0.698	0.47
Bandwidth (SWR < 1.5)	20 MHz	122 MHz	4.5 MHz	67 MHz	104 MHz	600 MHz
Gain		8.5 dB	7.7 dB	5.4 dB	8.6 dB	12.8 dB

LV-GSS/BPk..(tlv_feednew)...25/896

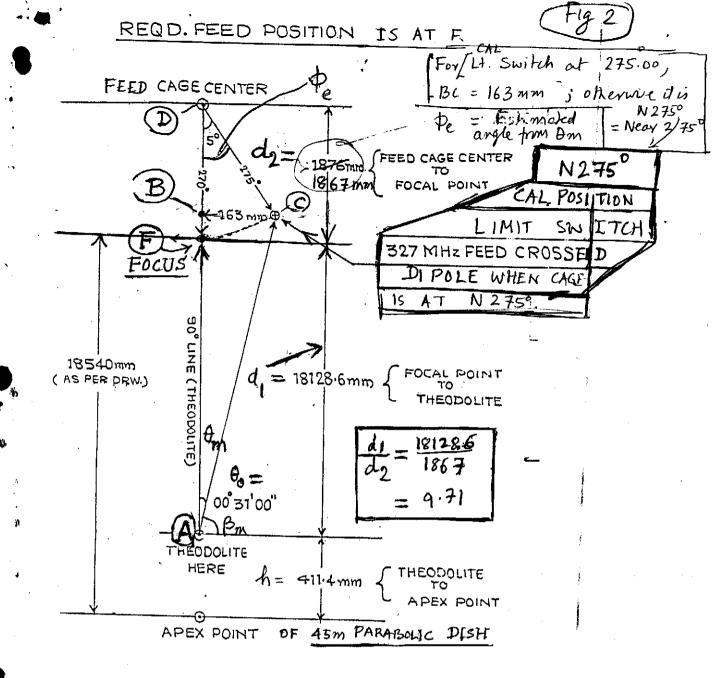


FIG.2: Shows the position of the 327 MHz
feed when fat the tot micro CAL microwatch position
The angle pe is required rotation angle of the

for positioning the feed to the Focal point.

The known constants d, and dz for 45-m

dishes and values of the as measured with

by placing a theodolik free the Apex of the

dish and sighting the 327 MHz feed when the

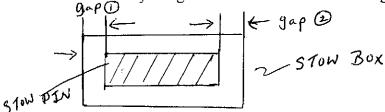
Cage hits the CAL micro-switch.

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PROCEDURE FOR THEODOLITE SURVEY FOR DETERMINING POSITION OF THE 327 MHz FEED WHEN THE FEED CAGE HITS THE CAL MICROSWITCH

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- From either the Control Room or bottom of the antenna being surveyed, rotate the Feed Cage till it hits the CAL micro-switch (i.e. CALIBRATE FPS). Note the FPS encoder value, which will be a bit higher than 17,000.
- 2. Bring the antenna to STP position and insert stowlock pins from Control Room or Shell. Measure approximately the gaps between the stowlock pins and stowlock box in the longer direction of the Box by using 1/2 or 1 mm shims or a Filler gauge.



3. Check alignment of the theodolite when it is on ground by measuring Az & El angles of a distant target both in FACE LEFT and FACE RIGHT. Both readings should be nearly the same. Any theodolite with at least 10 or 20 arcsec. accuracy and capability to use DIAGONAL EYE PIECE will do. It is preferable if the theodolite has optical readout for convenience of reading. If the Face left & Face Right readings have more than one arcmin difference, Feed Cage angles will have to be measured both along

Face Left and Face Right position of theodolite and a mean value taken. It is advisable to take both readings any case. In due course, the Theodolite adjustment may be done.

- 4. Place the Theodolite on the Theodolite Mount or Pipe stand at the APEX of the 45-m dish. (Make a rough sketch of the type of the Mount for record sake because there are more than one type of Mounts welded to the dish by V.M. Jog Engineering Ltd. and Southern Structurals Ltd.).
- 5. Level the theodolite and measure Az and Elevation angles of Node no. 12 for PRF 01, 03, 05, 07, 09, 11, 13, 15 and again for PRF 01 for cross-checking purpose. Face left and Face right readings are not required for PRF. Please note that PRF 01 and PRF 09 are along the Pin Sector direction. Record the readings in a Tabular format as per Enclosure-A. (Please note that the 45-m dish is in a "horizontal position" when the stowlock pin is inserted because of the method used for erection and alignment of the dish; the dish was lifted, levelled by surveying Nodes 12 & 17 for 8 or 16 frames and the stowlock pin was welded to the Yoke structure and then the inner surface of the dish inside the HUB was erected and adjusted). The above PRF measurement values will also cross check any departure of the dish from horizontal position and particularly also determine a small positional error of the 327 MHz feed in Azimuth. A separate Note is being written for reduction of the data.
- 6. Now inset the Diagonal Eye Piece on to the theodolite and measure Az and El angles of the centre of the crossed-dipoles of the 327 MHz feed. Take Face left and Face right readings as per Table A.
- 7. Height of the theodolite above the Apex of the dish is to be measured. It is expected to be 411 mm. If the Theodolite Mounts are intact and the height of the base-plate of the mount is available from previous records, it is sufficient to measure the height of

rotation axis of the theodolite telescope from the base plate. Otherwise measure the height with respect to the Elevation axis (see a sketch by Shri S. Rajmohan). An accuracy of about 1 cm is required.

8. Fig. 2 and Table 2 give a copy of the feed survey done by Shri Waman for general guidance

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ENCLOSURE-2

RELATION BETWEEN THE ANGLE θ_e OF THE FEED CAGE AND ANGLE θ_m MEASURED BY A THEODOLITE FOR THE 327 MHz FEED WHEN AT THE CALIBRATE (CAL) POSITION. ALSO, THE REQUIRED VALUE OF COUNTS OF THE FPS ENCODER FOR POSITIONING THE ANTENNA FEEDS.

- 1. Figure 2 shows the geometric relation between angles θ_m for the 327 MHz feed when at the CAL position.
- 2. The distance, d₁, between the focal point of 45-m dish, F, and rotation axis of the theodolite equals (18540-h), where h is the height of the theodolite above the Apex of the dish. The distance between the Apex of the 45-m dish and its focal point, F, equals 18540 mm as per TCE drawings. V.M. Jog Engineering Ltd. and Southern Structurals Ltd. have welded a permanent theodolite mount on many antennas, for which h = 411 mm. This needs checking w.r.t. elevation rotation axis and then by subtracting the height of the Apex w.r.t El rotation axis as per TCE drawings.
- 3. d₂ = distance between the centre of the rotation axis of the Feed Cage and the Focal point F.
- 4. The angle θ_m is the measured angle of the 327 MHz feed when at the CAL position w.r.t the vertical direction or zenith direction (see Fig.1). It is equal to $(90^{\circ}$ Elevation angle β_m as measured with a theodolite located above the apex point of the 45-m dish.).

- 5. The angle ϕ_e is the required rotation angle of the Feed Position System (FPS) drive for positioning the 327 MHz feed to the focal point.
- 6. We have the following relations:

BC =
$$d_2 \sin \phi_e$$
 (1)
also
BC = AB $\tan \theta_m$
= $(AF + FB) \tan \theta_m$

 $(d_1 + d_2 - d_2 \cos \phi_e) \tan \theta_m$

because FB = (DF - DB)

7. By equating (1) + (2), we get

Sin
$$\phi_e = \{(d_1 + d_2 (1 - \cos \phi_e)) \tan \theta_m \}/d_2$$
 (3)

If ϕ_e has a small value, $(1-\cos\phi_e)$ is nearly zero, and we can approximate value of ϕ_e as ϕ_e ' = $\sin^{-1}\left((d_1/d_2)\tan\theta_m\right)$ (4)

(2)

Where $d_1 = 18128 \text{ mm}$ and $d_2 = 1867 \text{ mm}$.

In the next iteration by inserting φ_e ' on RHS of Eq. 3, we can find more accurate value of φ_e

Since $\theta_m \leq 1^o$ and $\varphi_e \leq 10^o,$ we can also approximate

$$\phi_{e} = (18128/1867)\theta_{m}$$

$$= 9.71 \theta_{m} \tag{5}$$

This relation should be used only for a broad check.

8. For the FPS drive, one full rotation of 360° = 20, 480 counts of the incremental encoder (In fact, 360° = 5, 120 counts but the associated electronics multiplies the incremental encoder values by a factor of 4). Hence the required value of count, ΔN, corresponding to the angle φ_e is given by:

$$\Delta N_{327} = (20480/360) \phi_e$$
= 56.888 { $\sin^{-1} ((d_1/d_2) \tan \theta_m))$ }, or more accurately,
= 56.888 { $\sin^{-1} ((1/d_2) \times (d_1 + d_2 - d_2 \cos \phi_e) \times \tan \theta_m))$

and hence, the required value of counts of the incremental encoder for 327 MHz, N_{327}

$$N_{327} = (17,000 - \Delta N_{327})$$
 Counts (6)

9. Since 90° rotation = (20,480)/4 = 5,120 counts, hence

$$N_{610} = (N_{327} - 5120)$$
 Counts (7)
 $N_{150} = (N_{327} - 10240)$ Counts (8)
 $N_{1420} = (N_{327} - 15360)$ Counts (9)

$$N_{1420} = (N_{327}-15360)$$
 Counts (9)

10. It may be noted that an error of one Count = 1.05 arcmin. of the Feed Cage rotation and approximately (1.05/10.8) = 0.1 arcmin. of the 45-m antenna w.r.t. to the elevation axis. It is desirable that the positioning of the antenna feeds is within about ± 5 Counts on a repeatable basis, corresponding to ± 0.5 arcmin. or about (1/40th) of the beamwidth of 45-m dish at 1400 MHz.

(G. SWARUP)

24/11/1998

•	<u> </u>					1
•	-CURRE			70 enc	ANTENNAS	13 May 98 End.
(2	3	 		- Company of the Control of the Cont	
Ant name	Date Mon day Year	Mean dd ' " 	RMS arc m	Std.Dev arc min	90-(3)	Remarks
C00	24 Jul 1995 11 Aug 1995 20 Aug 1995 9 Sep 1995 26 Sep 1995 1 Oct 1995 14 Oct 1995 21 Nov 1995 4 Feb 1996 11 Mar 1996 25 Apr 1996 1 Jun 1996 1 Jun 1996 11 Jul 1996 21 Apr 1997 26 May 1997 17 Jun 1997 15 Sep 1997 26 Sep 1997 19 Apr 1998	89 44 11 89 44 25 89 44 36 89 44 27 89 45 47 89 44 11 89 44 21 89 44 21 89 43 58 89 43 55 89 44 20 89 43 55 89 44 10 89 43 14 89 44 14 89 44 0 89 44 5 89 44 20 89 43 44	8.45 8.53 8.71 8.66 8.77 8.60 8.64 8.24 1.69 2.14 1.21 1.93 Min 1.63 2.25 Min 1.63 2.25 2.23 2.80 2.46	2.99 3.01 3.08 3.06 3.10 2.53 3.05 2.93 2.21 2.38 0.69 0.96 0.54 0.79 0.81 0.92 0.58 0.91 1.98 1.01	89° 44'	norby Stable ruly 95 - Apr 98 Variation approx 89° 40' 15° 230'
C01 C01	5 May 1995 3 Aug 1995 11 Aug 1995 12 Sep 1995 16 Sep 1995 1 Oct 1995 14 Oct 1995 13 Nov 1995 13 Nov 1995 1 Feb 1996 11 Mar 1996 11 Mar 1996 11 May 1996 20 May 1996 20 Jun 1996 11 Jul 1996 20 Mar 1997 21 Apr 1997 4 Aug 1997 9 Aug 1997 15 Sep 1997	89 57 5 89 56 28 89 45 19 89 55 41 89 55 6 89 54 35 89 54 35 89 52 57 89 52 25 89 54 59 89 54 10 89 52 51 89 55 25 89 54 59 89 55 13 89 55 13 89 55 11 89 55 50	12.84 5.41 2.79 5.52 6.30 5.24 6.00 5.51 4.51 5.31 4.63 6.95 5.32 3.96 4.33 7.79 5.26 4.70 6.76 5.32 5.32 3.96 4.33 7.79 5.26 4.70 6.76 5.32 5.32 3.82	4.54 1.91 1.98 1.95 2.23 1.85 2.12 1.95 1.60 1.88 1.34 2.01 1.54 1.62 1.77 3.18 2.15 1.92 3.38 2.17 2.05 1.56	Seem from 80 - Pert Stors gap beha box Mean	old value No ho vari 990 52 to 37 5 Taps, Ha llage of took a larger i ren the structock and pin in 501.
C02 C02	1 Nov 1994 11 Nov 1994 25 Nov 1994 14 Feb 1995 16 Feb 1995 27 Feb 1995 15 Mar 1995 1 Apr 1995 8 May 1995 22 Jun 1995 24 Jun 1995 24 Jun 1995 24 Jul 1995 24 Jul 1995 2 Aug 1995 10 Aug 1995 20 Aug 1995	90 19 35 90 18 7 90 19 51 89 35 36 89 35 21 89 30 23 89 48 7 89 42 0 89 38 40 89 33 5 89 34 31 89 33 9 89 33 4 89 33 35 89 33 35 89 33 35 89 8 35	6.14 6.56 6.61 7.77 7.77 6.10 7.53 7.28 7.03 6.99 6.97 7.19 7.47 3.50 3.22 3.25	1.54 1.64 1.65 1.88 1.94 1.52 2.66 1.63 2.49 2.47 2.32 2.54 2.64 1.24 1.14	~ 90° 19' ~ 89° 33.5 89° 46' 89° 33.5	

C02	26 Aug	1995	89 25	15	3.54	1.25	1
C02		1995	89 25		3.10	1.10	
C02	· -	1995	89 25		3.16	1.12	
C02		1995	89 27	48	8.86	5.11	89° 25
C02		1995	89 24		3.17	1.12	89 23
C02		1995	89 25	54	3.29	1.16	
C02		1995	89 26		3.89	1.38	
C02		1996	89 26	33	4.47	1.58	† 1
C02		1996	89 25	9	4.03	1.42	
C02	1 Feb	1996	89 23	31	3.49	1.23	
C02	11 Mar	1996	89 25	13	3.95	1.14	
C02	7 Nov	1996	90 24	16	0.60	0.24	The state of the s
C02	23 Dec	1996	90 24	13	0.81	0.36	
C02		1996	90 24	32	0.81	0.40	
C02		1997	90 24	44	0.32	0.13	(
C02		1997	90 24	12	0.34	0.14	90° 24)
C02		1997	90 23	55	0.65	0.46	
C02		1997	90 24		0.82	0.34	hockoer
C02	1	1997	90 24		0.61	0.25	Club there
C02		1997	90 24		1.15	0.47	5 100
C02		1997	90 24	26	1.23	0.50	SCM 97 - Jan 10
C02		1997	90 23	35	0.88	0.63	To 98 0
C02		1997	90 23	35	0.88	0.63	Jan
C02		1998	89 53	55	4.86	1.98	Step there sep 97 - Jan 78 is and Jan 98 is Apr 32
C02		1998	89 53	55	4.86	1.98	
C02	Annual Security Comme	1998	89 53	55	4.86	1.98	
C02	19 Apr	1998	90 24	16	0.89	0.36	90° 24
C03	5 Jul	1994	90 0	16	6.68	1.53	· · · · · · · · · · · · · · · · · · ·
C03		1994	89 56	59	4.64	1.03	
C03		1994	90 0	25	5.58	3.03	
C03		1994	90 0		4.56	1.84	
C03		1994	90 0		3.67	1.91	
C03		1994	90 0		9.50	1.94	
C03		1994	90 0	32,	9.99	2.50	
C03	11 Nov	1994	90 0	45	9.19	2.30	
C03	23 Nov	1994	90 45	21	9.98	2.50	
C03	15 Feb	1995	90 42	45	15.66	3.80	
C03		1995	90 45	26	10.79	5.39	
C03		1995	90 45		11.08	3.92	
C03	:	1995	90 45	39	9.67	2.16	
C03		1995	90 45	32	9.94	3.51	
C03		1995	90 45	17	10.60	3.75	
C03		1995	90 45	32	11.47	4.05	
C03		1995	90 45	39	11.16	3.95	- step
C03		1995	89 56	3	11.99	4.24	1'
C03		1996	89 56	2	11.58	4.09	
C03		1996	89 56	6	10.56	3.73	
C03		1996	89 55	54	11.10	3.93	
C03		1996 1996	90 0 89 55	21 39	13.32	4.21	
C03		1997	89 55		1.18	0.48	
C03	,	1997	89 55	32 7	0.73	0.30	
C03		1997	89 55	20	1.79	0.49	
C03		1997	89 55	0	0.93	0.38	
C03	!	1997	89 55	38	1.76	0.72	aleh 1
C03		1998	90 22	13	T. Stranger	0.10	1-2011 32 re
C03		1998	90 22	13	0.24	0.10	- steh , 20° 22'
C04		1994	89 54		3.09	1.12	
C04		1994	89 56	2	5.89	1.46	
C04		1994	90 0	5	4.81	4.28	
C04		1994	89 59	45	5.77	1.29	
C04		1994	90 2		7.51	1.88	
C04		1994	90 14		7.93	1.98	
C04	23 Nov	1994	91 25	1	7.08	1.45	

C04	15 Feb	1995	91 24 5	6 8.87	2.22	, /
C04	27 Feb	1995	91 25 5	I	2.22	91° 25′
C04	2 Apr	1995	:	6 8.97	2.01	· · -
C04	1 May	1995	91 25 3		3.61	, ,
C04	8 May	1995	91 29 2	8.49	3.00	91 28 ± 2
C04	19 Jun	1995	91 30 1	0 7.05	2.49	
C04	24 Jun	1995	91 29 5	2 7.32	2.59	
C04	10 Jul	1995	91 28 4	5 9.86	3.48	
C04	l Aug	1995		8 9.67	3.42	
C04	20 Aug	1995	91 26 5		3.59	
C04	25 Aug	1995	90 0 1	,	2.67	
C04	9 Sep	1995	90 0 5	į.	3.35	, ,
C04	16 Sep	1995	90 0 4		3.77	9° 01 ± 2
C04	1 Oct	1995	90 1 4		3.21	90 01 12
C04	14 Oct	1995	90 1 2		2.60	
C04	7 Nov	1996	1	1 3.97	1.62	·
	23 Dec	1996	90 1 5	1 W 1777 17 17 17 17 17 17 17 17 17 17 17 1	1.46	Name of the Control o
C04	20 Mar	1997	89 59 5		1.78	
C04	27 May	1997	89 57 3		2.73	, ,
C04	18 Jun	1997	89 57 5		1.72	89° 58' ± 2'
C04	19 Jun	1997	89 56 1		2.74	
C04	11 Aug	1997	89 57 4!		2.21	Stable Mar-Sept 97
C04	15 Sep	1997	89 58 4		1.46	May-Slut 97
C04	26 Sep	1997	89 58 5	7 7.62	5.39	
1 COE		1007		7 1 06		- !
C05 C05	25 Apr	1997	89 49 5	,	0.80	
C05	26 May	1997	89 50 29	,	1.19	
C05	4 Aug	1997	89 49 50	,	0.42	89° 50' Stable
C05	15 Sep 19 Apr	1997 1998	!	1.38	0.56	
005		1990	89 49 31	2 0.65	0.27	89° 50' Stable May-Sept 93
C06	26 May	1997	89 58 19	9 0.41	0.17	-
C06	18 Jun	1997	89 58	:	0.17	
C06	4 Aug	1997	89 58 25		0.10	89° 58' Stable
C06	15 Sep	1997	89 57 4		0.30	87 38 State
			05 5, 4 	, 0,7% 	0.50	89° 58' Stable May-&ft9
C08	12 Aug	1997	90 7 39	9 1.07	0.44	· ' '
C08	26 Sep	1997	90 8 14		0.76	
C08	15 Feb	1998		0.00 ?		
C08	20 Feb	1998	90 7 53		1.38	
C08	19 Apr	1998	90 7 50		0.84	io stable Aug 97 -Apr 9
						50 Stable Ang 97 - Apr 9 90 08/ Stable Ang
C09	5 Jul	1994	89 46 7	7 6.24	2.56	1
C09	11 Jul	1994	89 47 59		2.14	
C09	15 Jul	1994	89 45 46		2.37	
C09	7 Sep	1994	90 15 2		2.73	
C09	6 Oct	1994			1.34	Many Class
C09	6 Oct	1994	89 44 (3.42	Mary Steps
C09	6 Oct	1994	89 44 15	•	3.31	•
C09	14 Feb	1995	89 45 48		3.31	
C09	15 Feb	1995	89 44 33	the fire with the profit of the fire and the profit of the	1.78	
C09	27 Feb	1995	89 43 50	•	1.48	0
C09	14 Mar	1995	89 43 25		2.17	
C09	1 Apr	1995	89 43 27		1.22	
C09	1 May	1995	89 44 38		2.10	
C09 C09	8 May	1995 1995	89 44 3		2.23	
C09	21 Jun 17 Jul	1995	89 44 53 89 41 42		2.20	
C09	31 Jul	1995	89 36 54		7.80	
C09	26 Aug	1995	89 26 1		2.15	*
C09	9 Sep	1995	89 24 31		2.15	
C09	16 Sep	1995	89 25 30		2.08	
C09	1 Oct	1995	89 25 18	1	2.13	l as a second here
C09	14 Oct	1995	89 24 24	ř	5.60	Slable Sept 95-Oct 96
C09	30 Oct	1995	89 23 53	:	2.13	"
C09	13 Nov	1995	89 24 39		2.23	
'	, , , , , ,		, 22 0.	1	1	' (

	l	400=					
C09	4 Dec 16 Jan	1995 1996	89 23 89 23	38 17	5.88	2.08	
C09	4 Feb	1996	89 22	18	5.96	2.15 1.72	
C09	11 Mar	1996	89 21	37	6.24	1.80	
C09	15 Apr	1996	89 21	27	6.10	1.76	(Step : Why)
C09	25 Apr	1996	89 21	44	0.43	0.18	*
C09 C09	20 May 7 Nov	1996 1996	89 22 89 17	32 52	0.16	0.06 0.86	ignore: Why wring?, 89° 17.3 ± 1
C09	25 Dec	1996	×89 12	0	18.31)	7.48	ianore why wring
C09	1 Jan	1997	89 17	48	0.55	0.28	
C09	25 Apr	1997	89 17	43	6.57	2.68	89 17.3 1
C09 C09	9 Aug	1997	89 16	27	p 1.07		Stable Dec 96-Apr 98
	19 Apr 	1998 	89 17 	13 	Kow 0.18	0.07	<u> </u>
C10	31 Dec	1996	90 17	17	3.52	1.44	
C10 C10	20 Mar 17 Jun	1997 1997	90 19	22 4	3.64 4.20	$1.48 \\ 1.72$	/
C10	26 Sep	1997	90 18	27	3.76	1.72	90°20
C10	19 Apr	1998	90 20	23	4.32	1.76	
C11	 20 Aug	1995	89 56	 52	3.56	1.26	_ -
C11	2 Sep	1995	89 56	13	3.55	1.26	
C11	23 Jan	1996	90 23	11	2.36	0.83	<u></u>
C11	1 Feb	1996	90 23	11	2.54	0.73	
C11 C11	11 May 20 Jun	1996 1996	90 23	53 28	0.76	0.31	
C11	20 Mar	1997	90 23	32	lov1.10	0.35 0.45	State
C11	25 Apr	1997	90 23	45	1.36	0.61	
C11	19 Jun	1997	90 23	20	0.87	0.35	$\downarrow \psi$
C11	11 Aug	1997	90 23	25	1.62	0.73	- Step: Why "
C11	19 Apr	1998 		32	0.79	0.32	stable Step: Why? 900 131
C12	5 Jul	1994	90 5	47	5.34	2.05	large errors
C12 C12	11 Jul 15 Jul	1994 1994	90 7	30 0	5.21 4.92	$2.54 \\ 1.12$	
C12	29 Jul	1994	90 6	9	3.89	1.85	large errors
C12	7 Sep	1994	90 5	30	(H)5.92	3.25	·
C12	4 Oct	1994	89 56	49	5.37	2.69	
C12	4 Oct	1994	89 59	10	hy/17.10	1.59	
C12 C12	1 Nov 11 Nov	1994 1994	90 0	5 42	7.65	1.91 1.85	
C12	22 Nov	1994	91 10	58	13.58	2.23	- I sucre
C12	24 Nov	1994	90 15	14	3.50	0.87	. 8
<u>C12</u>	5 Apr	1995	91 26	26	5.57	1.97	- ignore many
C12 C12	1 May	1995 1995	90 1 90 2	56 16	4.85 5.78	$\frac{1.72}{2.04}$	U
C12	20 Jun	1995	90 2	49	5.60	1.98	
C12	24 Jun	1995	90 2	11	4.27	1.51	
C12	10 Jul	1995	90 2	13	5.22	1.85	
C12 C12	31 Jul	1995	90 3	29 46	6.03	2.13	
C12	20 Aug 26 Aug	1995 1995	91 2	46 57	5.73 5.51	2.02 1.95	
C12	9 Sep	1995	90 23	6	5.39	1.91	
C12	1 Oct	1995	90 22	53	5.92	2.09	
C12	14 Oct	1995	90 22	⁵⁰ (L) 5.29	1.87	
C12 C12	30 Oct 13 Nov	1995 1995	90 22	3 \ 11	5.17	1.83 2.08	
C12	20 Nov	1995	90 22	$\frac{1}{4}$	4.42	1.56	_
C12	18 Jun	1996	90 22	40	0.36	0.16	72
C12	25 Dec	1996	90 10	9	30.79	12.57	Why large errors
C12	25 Dec	1996	90 10	<u>9</u> 45	30.79	12.57	
C12 C12	21 Apr 25 Apr	1997 1997	90 21	45 46	0.20 ? 4.52	0.10 1.85	1 90° 22' Stable
C12	4 Aug	1997	90 22	32	1.05	0.43	An 100 - Augax
C12	9 Aug	1997	90 22	17	1.33	0.54] why large errors?? 30° 22' stable Apr 93 - Aug 9x
					- / ~~		_

-	_		_		_			-	•
S01 S01	E03 E03 E03	E03 E03 E03	E02 E02 E02 E02 E02 E02	W04 W04 W04 W04 W04	W03 W03 W03	W02 W02 W02 W02 W02 W02 W02 W02	W01 W01 W01 W01 W01 W01	C14 C14 C14 C14 C14 C14 C14 C14 C14 C14	C13 C13 C13 C13 C13 C13 C13
15 Fe 20 Fe	13 Ja 15 Fe 20 Fe	25 De 1 Ja 11 Au	16 De 11 Au 13 Ja 6 Fe 15 Fe 20 Fe	13 De 13 De 30 De 25 Ap 10 Ma	4 De 19 Ju 12 Au	2 De 4 De 20 Ma 21 Ap 25 Ap 10 Ma 19 Ju 4 Oc	6 Se 25 Se 17 Oc 2 No 1 Fe 20 Ma 13 De	1 No 20 No 1 Fe 1 Ju 14 Ju 11 Ju 5 De 31 De 20 Ma 25 Ap 11 Ma 11 JU 15 Se 19 Ap	1 Ju 2 De 4 De 1 Ja 11 Ma 26 Ma
	b 199	n 199 g 199	g 199 n 199 b 199 b 199	c 199 c 199 r 199 y 199	n 199	r 199 r 199 r 199 r 199 y 199 n 199	p 199 t 199 v 199 b 199 y 199	v 199 b 199 n 199 n 199 c 199 c 199 r 199 y 199 N 199 p 199	c 199 c 199 n 199 y 199
	8	7 「 7	7 8 8 8	6 7 7	7	6 7 7 7 7 7	5 5 6 6	5 6 6 6 6 6 6 7 7 7 7	6 6 7 7
90 90	90 90 90	89 90 90	90 90 90 90 90	90 90 90 90 90	90 90 90	89 89 89 89 89 89	90 90 90 90 90 90	90 90 90 89 90 89 89 89 89 89	89 89 89 89 89
11 35	2 1 1	53 2 2	19 19 18 18 19 19	20 20 20 21 21	20 22 22	56 56 55 55 56 55 55	13 17 17 17 16 17	6 5 5 51 1 44 45 45 43 44 33 59 24 23	40 37 38 36 35 33
29 40	4 39 46	4 15 58	15 40 0 51 0 5	52 54 9 27 48	43 44 26	14 2 55 59 7 36 49	20 31 14 15 18 15	44 1 34 50 22 52 39 27 53 2 6 50 25 36	32 24 2 41 19 57
41.24	1.42 2.01 1.92	26.64 1.59 1.49	5.63 6.30 8.98 9.37 9.56 8.33	2.87 0.39 1.05 0.40 0.63	2.87 1.47 1.65	0.55 0.75 0.67 0.70 0.75 0.67 0.45 0.63	2.59 2.69 2.85 2.93 7.20 3.22 2.66	1.89 1.81 2.18 0.91 1.90 2.89 2.35 2.02 2.62 2.45 2.40 2.40 (H) 3.22	0.44 0.60 0.12 0.48 0.85 0.76
23.81	0.58 0.82 0.79	10.87 0.65 0.61	2.30 2.57 3.67 3.82 3.90 3.40	1.17 0.16 0.47 0.16 0.31	1.66 0.60 0.74	0.22 0.31 0.27 0.35 0.31 0.34 0.18	0.92 0.95 1.01 1.04 1.12 1.31	0.67 0.64 0.63 0.41 0.78 1.18 0.96 0.90 1.07 1.00 2.35 2.35 0.73 1.31	0.20 0.30 0.07 0.24 0.43
+ W	1 90	1 WITE		 			98	Ste W	
rong me - 90° =	2	p large wron	,			19° 56	6 1 5 13	y? arse err	Pradue Why
2as ! 36	error? y mees stable Tan 97 - 2as?	error!	0				Stabb Sept 9		l shift
	Fel-98	?					e 5 - Dec 98	ið-Αþr &	

Antenna No.	Theodolite No	Measured by	Date	Time
ı, surve	Y OF PRF			
 PRF No.	Azimuth		Vation	
	(Node 12)		ode 12)	·
01				
03				
05				
07				
09				
11				
13				
15				
Av of El				
only				
Av of Az of PF	UF .			
01 to 09				

2. THEODOLITE MEASUREMENTS OF 327 MHz FEED IN CAL POSITION a) Put antenna in stowlock position from control room or base of the antenna. Measure the gaps on long side between the stowlock position and stowlock box using 1/2 or 1 mm shims. b) Put 327 MHz feed in CAL position from Control room or base of the antenna. Sr. Azimuth Elevation No. 1. Face Left 2. Face Right 3. Face Left 4. Face Right 5. Face Left			
Measure the gaps on long side between the stowlock position and stowlock box using 1/2 or 1 mm shims. b) Put 327 MHz feed in CAL position from Control room or base of the antenna. Sr. Azimuth Elevation No. 1. Face Left 2. Face Right 3. Face Left 4. Face Right 5. Face Left	2.	THEODOLITE MEASUREMENTS OF 327	
Sr. Azimuth Elevation No. 1. Face Left 2. Face Right 3. Face Left 4. Face Right 5. Face Left	Mea	sure the gaps on long side between the stowlock	ntrol room or base of the antenna. position and stowlock box using 1/2
Sr. Azimuth Elevation No. 1. Face Left 2. Face Right 3. Face Left 4. Face Right 5. Face Left	b)	Put 327 MHz feed in CAL position from Cont	trol room or base of the antenna.
 Face Left Face Right Face Left Face Right Face Left 		Azimuth	Elevation
 3. Face Left 4. Face Right 5. Face Left 	1.		
4. Face Right 5. Face Left	2.	Face Right	
5. Face Left	3.	Face Left	
	4.	Face Right	
5. Face Right	5.	Face Left	
	6.	Face Right	

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